

PROCESS AMENABILITY TEST OF LOW GRADE IRON ORE

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ABSTRACT: Utilisation of Low-Grade Iron Ore Fines after concentration not only helps in conservation of the mineral wealth, but also substantially improves the economics of iron ore mining. There has been need to develop suitable beneficiation process for upgradation of low-grade iron ores towards their rational utilisation. Presently the circuit adopted for processing iron ores has limitations in reduction of alumina. The depletion of high-grade reserves, utilisation of low-grade reserves coupled with increasing market pressure for improved product quality necessitates re-examination of the process flow sheets and evaluate alternative or supplemental processing routes. The main objective of the Process amenability studies for utilisation of Low-Grade Iron Ore Fines (-10mm) is to get Pellet grade concentrate with +65% Fe (min), SiO₂ 1.8% (max), Al₂O₃ 1.8% (max) and other proportionate constituents by adopting suitable beneficiation techniques and to collect the relevant data (Quality and Quantity of the Products) for the process development. In an effort to formulate a conceptual process flow sheet, the Process amenability studies for utilisation of Low-Grade Iron Ore Fines (-10mm), which is lying at a mine site in India, samples were collected and taken up for the study. The efforts of R & D of NMDC are discussed in this paper. Low-Grade Iron Ore Fines (-10mm) sample assayed 60.10% Fe with 3.48% SiO₂ and 4.48% Al₂O₃. Microscopic examination reveals that the grain sizes of the ore minerals are varying from 40 to 300 microns. The sample consists of hematite as the chief ore mineral followed by minor amounts of magnetite. The gangue minerals include quartz and ferruginous clay in which quartz occurs as medium grained where as ferruginous clay occurs as fine to sub microscopic size mineral. The economical

processing route evolved out of the studies finally could yield a final concentrate constituting 58.63% by weight along with Iron unit's recovery of 63.51% assaying 65.10% Fe with 1.48% SiO₂ and 1.85% Al₂O₃. The economical processing route that adopted comprises the following operations. Making slurry in a sump pump followed by grinding in close circuit with 48mesh size Screen. The – 48 mesh size product was subjected to the Cycloning to remove slimes. The Cyclone Underflow product was subjected to Floatex Density Separation (FDS) to separate fine heavy minerals from the gangue minerals. The FDS Underflow was collected as concentrate. The FDS Overflow product was further subjected with Wet High Intensity Magnetic Separation (WHIMS) to recover more Iron units as magnetics. A conceptual process flow sheet was evolved, which may become the prelude to the subsequent finalisation of the process flow sheet for commercialisation.

1.INTRODUCTION

Iron is the second most common metallic element found in the crust of the Earth and makes up 5.6 percent of the lithosphere. Iron's most important minerals are its oxides (hematite and magnetite), hydroxides (limonite and goethite), carbonates (siderite), and sulphides. Hematite and magnetite are examples of iron oxides (pyrite). Iron, like the majority of other metals, can only be found in the crust of the Earth in the form of an ore, which means that it is coupled with other elements like oxygen or sulphur. Iron may be obtained from a variety of different ores, but the two most significant ones are hematite and magnetite. Hematite, on the other hand, is seen as being superior than magnetite due to the fact that it has larger deposits than magnetite does, and the majority of magnetite resources are located in dense forests, rendering them inaccessible for

industrial use. The production of iron and steel starts with the most fundamental raw material: iron ore. Depending on the grade, the amount of carbon that is present in steel may range from 0.2 percent to 2.1 percent by weight. Steel is an alloy that is mostly made up of iron. In order to extract iron from its ore, oxygen must first be removed, and then there must be combined with a chosen chemical partner such as carbon. Smelting is the term used to describe this process.

1.1 Iron Ore Fines:

The typical particle sizes of the ore used in rotary kilns range from 5 to 18 millimetres. Crushing and screening the lumpy ore that is obtained from the mines results in the production of this size range of the ore. As a result of this operation, practically all of the ore is generated in the form of fines. Nearly 0.8 tonnes of iron ore fines are required for every tonne of sponge iron that is manufactured. The following is an example of an iron ore fines sieve analysis:

1. -1mm (30-40%)
2. -3mm (35-38%)
3. +3, -5mm (28-45%)

Utilization of Iron Ore Fines:

The following is a list of potential applications for the Iron Ore Fines that are generated as a waste material: By modifying the positive size of the coal, etc., some amount of between +3 and -5mm may be employed together with the charge in the rotary kiln. The iron ore fines may be pelletized and then used in either the blast furnace or the rotary kiln in the process of creating pig iron or sponge iron, respectively. Iron ore fines may be used to make sinters, which can then be put into the blast furnace. For use in an electric arc furnace (EAF) or an iron blast furnace, composite pre-reduced pellets (CPR) may be manufactured from coal fines and iron ore. Iron ore fines in coal may be used to make various types of

sponge iron products, such as rods, granules, and so on. The features of the raw materials that are used in the manufacturing of DRI are very important to consider due to the close relationship between efficiency and cost effectiveness. These aspects are controlled by the characteristics of the coal used in the process. For the purpose of selecting iron ore for the DR process, the following criteria are taken into consideration.

1. The Constituents of Chemicals
2. The ability to be reduced
3. Physical Attributes (such as Height, Weight, and Strength).

Aim of Present Work and Its Scope:

AIM: Beneficiation studies were conducted on a ore sample that weighed about 600 kilograms and had an analysis of 40 percent iron and 36 percent silicon dioxide. The sample came from the Sanjeevarayana Kote village in the Bellary (Tq) (Dist) region of Karnataka. The goal of the studies was to produce a pellet grade concentrate that contained more than 64 percent iron.

The scope of work comprises:

- A sample of the size distribution of the feed.
- Examining the sample for its physical and chemical characteristics once it has been received.
- Feasibility studies on mineral processing for the purpose of lowering the silica content in the as received sample as much as is humanly feasible and raising the iron content to a level more than 64 percent while maintaining the highest possible iron recovery and grade.
- The optimization of settings for the Davis Tube test, such as the mesh of the grind, in order to conduct a study of percent magnetics

□ Studies of magnetic separation using a drum first, then studies of magnetic separation using a wet high intensity magnet.

□ The preparation of the material and maintenance of metallurgical balance.

Objective:

The purpose of this research is to improve the quality of low-grade magnetite ore by performing amenability studies on the effects of particle size on magnetic separation processes. These processes included drum magnetite separation, wet high and low intensity magnetic separation, and vertical pulsating high gradient magnetic separation. The end goal is to produce a pellet-grade concentrate that has a high grade and high recovery.

II. LITERATURE REVIEW

The characteristics of the ore deposits, in particular the grain size of the mineral value in the ore, its dissemination in the mass of the deposit, and its association with the gangue minerals, play a significant role in determining the liberation size, the abundance of fine particles, the selection of efficient equipment, the appropriate separation method in some cases, and, as a consequence, the entire flow sheet of ore processing. Because the minerals are freed at relatively coarse sizes in high-grade deposits, there is no need for extensive particle size reduction to be carried out in these deposits. As a consequence of this, the proportion of tiny particles is often rather low, and the objective of the whole process is to achieve the greatest possible degree of release while working with a particle size range that is as coarse as is practically feasible. In the event that the coarser particles cannot be effectively separated from the finer particles, the finer particles must be eliminated before the beneficiation process can begin on the coarser particles. The separation of fine particles has been the subject of intensive research for a good number of years [11-13]. Banded magnetite quartzite (BMQ) ore occurs as separate are considered to be low grade iron

ores with Fe content of 25–45 percent, SiO₂ content of 30–60 percent, and Al₂O₃ content of 1–5 percent. Despite the difficulty of processing fine and ultrafine nature banded magnetite quartzite (BMQ) ore occurs as separate. To date, there is not a single commercial facility that has been established to extract the iron values from these ores for use in any industrial processes. However, because of the growing demand for high-quality iron ore from the iron and steel industries and the depletion of high-grade ores, it has become imperative to maximise the use of low-grade ores by the use of appropriate beneficiation processes. Methods such as gravity concentration, magnetic separation, and flotation are often used in an effort to increase the amount of iron that can be extracted from ores with such a low grade. Therefore, the processing of finely dispersed mineral particles requires either an upgrade or modification of the current separation methods, as well as the adoption of novel approaches. This research provides a summary of the progress that has been made in the techniques of separation (physical and physicochemical) as well as the creation of new pieces of equipment to deal with the challenge of separating small particles. In the end, an investigation into the use of a variety of magnetic processing techniques for low-grade magnetite ores is presented.

III. RAW MATERIALS

Sample of Ore The low grade iron ore sample that was utilised in this inquiry came from Sanjeevarayana Kote village in Bellary, Karnataka. It was used in this investigation since it was available. As can be seen in Figure 3, this deposit is a component of a banded iron ore formation



Fig 1. Iron ore sample forms for study area

Physical Examination:

In accordance with the findings of the physical investigation, the majority of the sample was composed of brown fines, while only a trace quantity was comprised of hard, compact chips measuring less than one millimetre in size (see Figure 4). And demonstrated a specific gravity of roughly 4.8 and an angle of repose of 42 degrees.



Fig2. Feed Sample

Chemical Analysis.

After being reduced to the required size, a representative piece of the sample as it was received was then submitted to a comprehensive chemical analysis. Figure 5 shows the findings of the chemical analysis performed on the material in its as-received state.

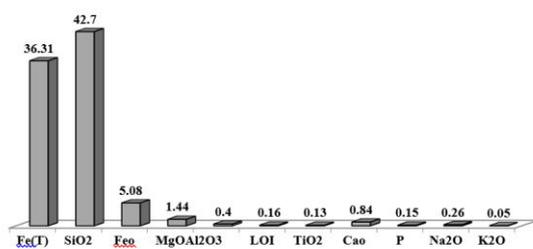


Fig3. Chemical analysis of as received sample

Mineralogy:

The examination of the sample with a stereo microscope reveals that the sample primarily consists of hematite and magnetized magnetite, along with major amounts of quartz and very minor amounts of goethite/limonite and ferruginous clay, as shown in figure 6. The majority of the quartz grains have fine

inclusions in them, as the studies with the stereo microscope show.

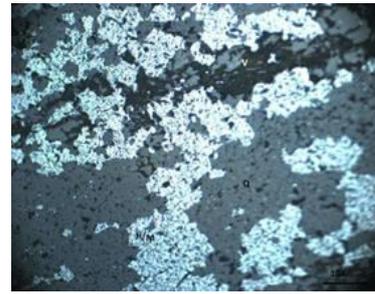


Fig.4 Stereo Micrograph of As received Sample showing Hematite/Magnetite and Quartz(10X)

Feed preparation and sampling

For the purpose of this investigation, an approximately 500-kilogram sample of the low-grade iron ore found in the study region was collected. As shown in Figure 7, a representative sub sample was taken from the bulk sample by using riffle sampling as well as coning and quartering. A subsample was taken for the experiment, and it was sieved to determine what percentage of particles were larger than 100 mesh (150 microns). Following that, the sample was used for characterization studies, which included particle size analysis (dry and wet), chemical analysis, and amenability studies. The remaining sample was put to use for beneficiation research.



Fig.5 Sub Sampling of Feed

IV. RESULTS AND DISCUSSIONS

4.1 Drum magnetic separation studies

The as received sample of about 600 kg was carefully mixed before being put into the drum magnetic separation device. This was done in order to separate the magnetic fraction from the non-magnetic fraction in the feed material. According to the findings, around

thirty percent of the overall volume was considered to be a non-magnetic fraction. In addition, representative samples of Mag products totaling 250 grammes were analysed using a wet sieve in great detail. The precise size distribution as well as the amount of Fe present in each Mag product fraction is shown in Table.4. Additionally, it was discovered that almost 33 percent of the Drum mag product is composed of +100 Mesh (150 Microns). According to the findings, the grade of the drum product is at its highest point at a finer size, namely at -200 mesh, where it contains 62 percent iron.

Mesh no	microns	Wt%	Cum wt% passing	Fe%	Fe Distr	SiO2	Al2O3	LOI	FeO
+100#	150	32.37	67.63	46.35	26.98	30.84	0.11	-	5.28
+150#	106	20.28	47.35	57.06	20.81	16.23	0.10	-	6.83
+200#	75	19.26	28.09	61.00	21.13	10.92	0.08	-	5.33
+250#	63	8.12	19.97	61.75	9.01	9.37	0.08	-	5.56
+325#	53	11.68	8.29	62.98	13.23	7.94	0.08	-	6.31
+400#	45	2.45	5.84	62.94	2.77	7.87	0.09	-	6.42
-400#	38	5.73	0	58.78	6.05	12.26	0.16	0.61	7.90
Head		100.0		55.60	100.0				

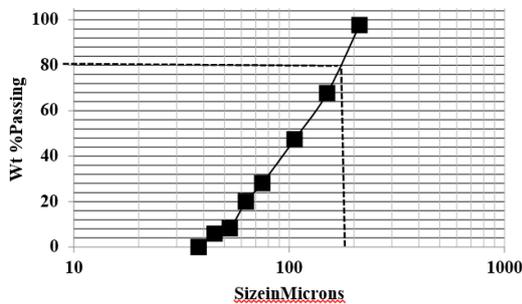


Fig.6 Size analysis of as received sample

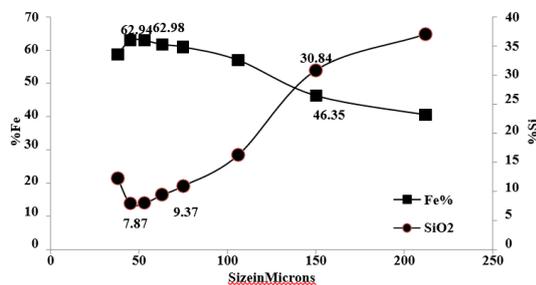


Fig.7 Effect of Size on %Fe and %Si values of feed sample

4.2 Effect of MOG on Davis Tube Test

Wet grinding was performed on a representative sample that weighed close to

200 grammes of feed for a period of time that ranged from 5 to 20 minutes. The ground goods were put through the Davis tube test, which has a water flow rate of 650 cc/min and is designed to keep the pulp level in the tube and at the poles at a constant level. The agitation rates start at 30 revolutions per minute (RPM). Ten minutes had been allotted for the agitation time. The slope angle of 45 degrees has been chosen for the investigation. The tabulated findings may be seen in Table 5.

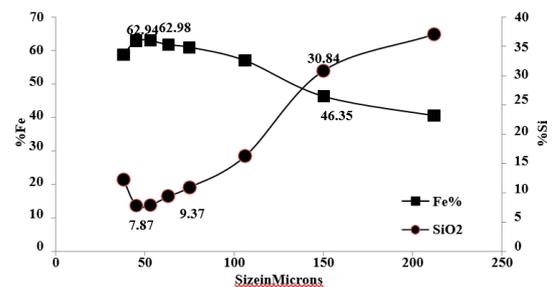


Table. Davis tube test results

Sr no	Grinding time	products	Wt in gms	Wt %	Fe%	Distn (%Fe)
1	0 Min (D ₈₀ -1mm)	Mag	17	56.67	45.3	60.00
		Non-Mag	13	43.33	39.5	40.01
		Head	30	100	42.78	
2	5 minutes (D ₈₀ -0.6mm)	Mag	18.5	61.67	47.8	65.36
		Non Mag	12.5	41.67	40.2	37.14
		Head	30	100	45.1	
3	10 minutes (D ₈₀ -0.3mm)	Mag	15.8	52.67	55.9	58.24
		Non Mag	14.2	47.33	39.7	37.17
		Head	30	100	50.55	
4	15 minutes (D ₈₀ -0.1mm)	Mag	14	46.67	62.8	52.31
		Non Mag	16	53.33	40.2	38.27
		Head	30	100	56.02	
5	20 minutes (D ₈₀ -0.075mm)	Mag	13.5	45.00	64.5	49.64
		Non Mag	17.5	58.33	40.4	40.31
		Head	30	100	58.47	

V. SUMMARY AND CONCLUSION

A Banded Magnetite Quartzite (BMQ) sample with a number of -150# was obtained from the Sanjeevarayana Kote hamlet in the Bellary area. This sample was used in a process evolution to get concentrate with an assay of Fe > 65 percent. The pre-concentrated sample had an analysis of 37 percent Fe(T) and 42 percent silica content, with the majority of the silica coming from fine grind magnetite and fine grind quartz. The process amenability test suggested that a MOG with a finer particle size than -100 # should be separated using magnetic forces in order to create the concentrate of the required grade.

The exploratory Davis tube test provided confirmation of the result of the amenability test in relation to MOG. The results of the tabling test on extremely MOG revealed that

the necessary grade concentrate could be generated only at MOG finer than -150 mesh, despite the fact that recovery was low. In a similar manner, LIMS confirming -100# MOG results in 66.6% Fe with 74.6% Distribution.

According to the findings of the research relevant to LIMS non mag that was submitted to WMIMS validating MOG, -200#, MOG is necessary for the production of the required grade concentrate.

The VPHGMS test is carried out with the goal of recovering the tiny Magnetic fractions from the tails of the whole process, which gives a total of 49 percent Fe with 23 percent dispersion.

The final flow sheet is illustrated in figure, and it produces a concentrate that has a Fe content of 64.67 percent, with a Fe distribution of roughly 70 percent at a Wt percent yield of 74. The product satisfies the requirements of the given standard in addition to those of the metallurgical industry (with reference to Fe) and the Heavy media specification.

It is advised that a detailed combination test on a continuous pilot scale test be performed for the purpose of confirming the process, enhancing it, and collecting engineering data for the conceptual plant. In light of the fact that the material investigation of amenability processing.

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